

### Combined Footing Verification Example

Reference: Reinforced Concrete – Mechanics and Design, 5<sup>th</sup> Edition, by Wright and MacGregor, Prentice Hall, 2009. Example 15-4.

A combined footing supports an 24-in x 16-in exterior column carrying a service dead load of 200 kips and a service live load of 150 kips, plus a 24-in square interior column carrying service loads of 300 kips dead and 225 live. The distance between the columns is 20-ft center to center. The allowable soil bearing pressure is 5000 psi at a depth of 4-ft below the finished floor. The density of the fill above the footing is 120 pcf. Design the footing assuming  $f'_c = 3$  ksi and  $f_y = 60$  ksi.

The resultant of the column loads is located at a distance:

$$(8 \times 350 + 248 \times 525) / (350 + 525) = 152'' \text{ from the exterior face of the exterior column.}$$

- Try a combined footing 25'-4" long x 8'-0" wide x 3'-4" thick. The factored net pressure is:

$$q_{nu} = (1.2 \times (200 + 300) + 1.6 \times (150 + 225)) / (25.33 \times 8) = 5.92 \text{ ksf}$$

$$\text{Max. shear at CL of ext. column} = 5.92 \times 8 \times 0.67 - 1.2 \times 200 - 1.6 \times 150 = 448 \text{ kips}$$

$$\text{Max. shear at CL of int. column} = 5.92 \times 8 \times 4.67 - 1.2 \times 300 - 1.6 \times 225 = 499 \text{ kips}$$

$$\text{Distance of zero shear from CL of ext. column} = 20 / (448 + 499) * 448 = 9.45 \text{ ft}$$

$$\text{Maximum bending moment} = 5.92 * 8 * 0.67^2 / 2 - 448 * 9.45 / 2 = 2106 \text{ k-ft}$$

- Check punching shear at interior column.

The critical perimeter is a square with sides  $24 + 36.5 = 60.5''$

$$V_u = 1.2 \times 300 + 1.6 * 225 - 5.92 * (60.5 / 12)^2 = 569 \text{ kips}$$

$$\phi V_c = 0.75 \times 4 \sqrt{3000} \times 60.5 \times 4 \times 36.5 = 1451 \text{ kips} > V_u, \text{ Ratio} = 0.40 \text{ OK}$$

- Check punching shear at exterior column.

The critical perimeter is three sided  $24 + 36.5 + 2(16 + 36.5/2) = 129''$

$$V_u = 1.2 \times 200 + 1.6 * 150 - 5.92 * (24 + 36.5)(16 + 36.5/2) / 144 = 395 \text{ kips}$$

$$\phi V_c = 0.75 \times 4 \sqrt{3000} \times 129 \times 36.5 = 774 \text{ kips} > V_u, \text{ Ratio} = 0.52 \text{ OK}$$

- Check one-way shear in the longitudinal direction at distance  $d$  from the interior column face.

$$V_u = 499 - 5.92 * 8 * (12 + 36.5) / 12 = 308 \text{ kips}$$

$$\phi V_c = 0.75 * 2 * \sqrt{3000} * 96 * 36.5 = 286 \text{ kips} < V_u, \text{ Ratio} = 1.08 \text{ NG}$$

Either use min additional shear reinforcement or increase  $f'_c$  to 3.5 ksi.

- Design flexural reinforcement in the longitudinal direction.

$$M_u = 2106 \text{ k-ft. Try 19 \#8 bars at top } (A_s = 15.0 \text{ in}^2)$$

$$a = 15.0 * 60 / (0.85 * 3 * 96) = 3.67 \text{ in (tension controlled)}$$

$$\phi M_n = 0.9 * 15.0 * 60 (37.5 - 3.67/2) / 12 = 2408 \text{ k-ft} > M_u, \text{ Ratio} = 0.87 \text{ OK}$$

$$\text{Use 15 \#8 bars at bottom } (A_s = 11.9 \text{ in}^2)$$

- Check the development of top bars.

The clear spacing exceeds  $2d_b$  and the clear cover exceeds  $d_b$ , therefore

$$L_d = 1.3 * 60000 / (20 * \sqrt{3000}) d_b = 1.3 * 54.8 * 1" = 71.2" \text{ OK}$$

- Design the transverse bars.

$$\text{The factored interior load is } 1.2 * 300 + 1.6 * 225 = 720 \text{ kips}$$

$$\text{This is balanced by a net upward force of } 720 / 8' = 90 \text{ k/ft}$$

$$M_u = 90 * 3^2 / 2 = 405 \text{ k-ft. Try 9 \#8 transverse bars at bottom } (A_s = 7.11 \text{ in}^2)$$

- Design the column-footing joint.

$$\text{The allowable bearing on the interior footing is } 0.85 * 0.65 * 3 * 24^2 * 2 = 1909 \text{ kips}$$

$$\text{The allowable bearing on the base of the column is } 0.85 * 0.65 * 3 * 24^2 = 955 \text{ kips} > P_u = 720 \text{ kips OK}$$

$$\text{Area of dowels minimum} = 0.005 * 24^2 = 2.88 \text{ in}^2 \text{ (controls)}$$

Use 8 #6 dowels. Extend dowels 25" into column.

**GEOMETRY**

Column to Column Distance	20.00	ft	
	<u>Exterior</u>	<u>Interior</u>	
Column Length (X)	16.0	24.0	in
Column Width (Z)	24.0	24.0	in
Edge Distance (X)	0.67	4.66	ft OK
Footing Width (Z)	8.00	8.00	ft
Footing Thickness	40.0	in	OK
Soil Cover	0.67	ft	
Pedestal Height	N. A.		

**SOIL PRESSURES (Comb: D+L)**

Gross Allow. Soil Pressure	5.00	ksf	
Overburden Pressure	0.58	ksf	
Reaction Force	992.1	kip	
Reaction Eccentricity	0.00	ft	
Ftg. Area in Contact with Soil	100.0	%	
	<u>Exterior</u>	<u>Interior</u>	
Bearing Pressure	4.89	4.90	ksf
Bearing Ratio	0.98	0.98	OK

**APPLIED LOADS**

- Exterior Col.	Dead	Live	RLive	Snow	Wind	Seismic	
Axial Force P	200.0	150.0	0.0	0.0	0.0	0.0	kip
Moment about Z Mz	0.0	0.0	0.0	0.0	0.0	0.0	k-ft
Shear Force Vx	0.0	0.0	0.0	0.0	0.0	0.0	kip
- Interior Col.	Dead	Live	RLive	Snow	Wind	Seismic	
Axial Force P	300.0	225.0	0.0	0.0	0.0	0.0	kip
Moment about Z Mz	0.0	0.0	0.0	0.0	0.0	0.0	k-ft
Shear Force Vx	0.0	0.0	0.0	0.0	0.0	0.0	kip

**MATERIALS**

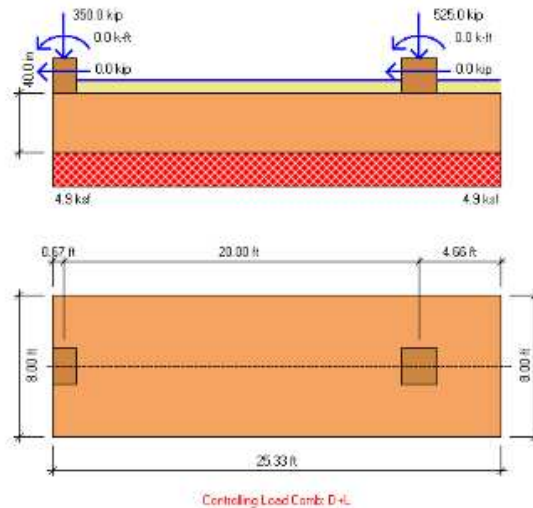
	Columns	Footing	
Concrete fc	4.0	3.0	ksi
Reinf. Steel fy	60.0	60.0	ksi
Soil Cover Density		120.0	pcf

**SLIDING (Comb. 0.6D+1W)**

Footing-Soil Friction Coeff.	0.45	
Passive Pressure Coeff. Kp	2.77	
Friction Force at Base	166.6	kip
Passive Force @ Ftg	20.7	kip
Horiz. Resisting Force	187.3	kip
Horiz. Sliding Force	0.0	kip
Sliding Safety Factor	99.99 > 1.5	OK

**DESIGN CODES**

Concrete Design	ACI 318-08
Load Combinations	ASCE 7-05



**OVERTURNING CALCULATIONS (Comb: 0.6D+1W)**

OVERTURNING				RESISTING			
	Force	Arm	Moment		Force	Arm	Moment
- About Z-Z	kip	ft	k-ft	- About Z-Z	kip	ft	k-ft
Ext. Moment Mz ...	0.0	0.0	0.0	Soil Cover .....	9.5	12.67	119.7
Ext. Shear Vx .....	0.0	3.33	0.0	Footing Weight ...	60.8	12.67	769.9
Int. Moment Mz ....	0.0	0.0	0.0	Ext. Column .....	0.0	24.66	0.0
Int. Shear Vx .....	0.0	3.33	0.0	Int. Column .....	0.0	4.66	0.0
Rh =	0.0	OTM =	0.0	Ext. Axial P .....	120.0	24.66	2959.2
Arm of Vertical Resultant ....	12.66	ft		Int. Axial P .....	180.0	4.66	838.8
Overturning Safety Factor ..	99.99	> 1.5	OK	Rv =	370.2	RM =	4687.7

**FOOTING AT EXTERIOR COL.**

**- One-way Shear (Comb: 1.2D+1.6L+0.5S)**

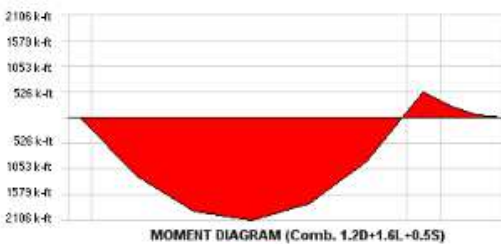
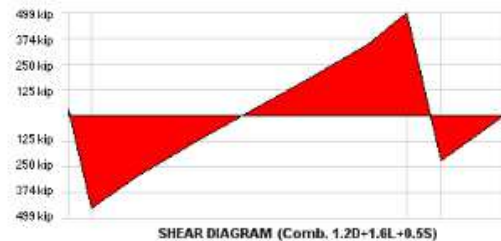
	- Side	+ Side
Under-strength $\phi$ Factor .....	0.75	
One-way Shear Vux ...	0.0	101.3 kip
Shear Strength $\phi V_{cx}$ ..	283.9	283.9 kip
Max. One-way Shear Ratio $V_u/\phi V_c$ ..	0.36	OK

**- Punching Shear (Comb: 1.2D+1.6L+0.5S)**

Unbalanced Moment Factor $\gamma_{vx}$ ...	0.33
Punching Shear due to Axial ....	85.9 psi
Punching Shear due to Mz .....	0.0 psi
Punching Shear Stress $V_u$ .....	85.9 psi
Effective Perimeter $b_o$ .....	128.1 in
Average Effective Depth $d$ .....	36.0 in
Punching Shear Strength $\phi V_c$ ..	164.3 psi
Punching Shear Ratio $V_u/\phi V_c$ .....	0.52 OK

**- Transv. Flexure (Comb: 1.2D+1.6L+0.5S)**

	Top	Bot
Under-strength $\phi$ Factor .....	0.90	
Footing Effective Length .....	5.00 ft	
Use 6 #6 Bars Parallel to Z (Top) , $d = 36.6$ in		
Use 6 #8 Bars Parallel to Z (Bot) , $d = 35.5$ in		
Bottom Steel Min. Area Ratio .....	0.91 OK	
Bending Moment Mux ...	0.0	284.1 k-ft
Bending Strength $\phi M_{nx}$	428.9	737.3 k-ft
Max. Bending Ratio $M_{ux}/\phi M_{nx}$ .....	0.39	OK
Top Z-Bars Develop. Length Ratio ,	0.00	OK
Bot Z-Bars Develop. Length Ratio ..	0.37	OK





**FOOTING AT INTERIOR COL.**

- One-way Shear (Comb: 1.2D+1.6L+0.5S)

Under-strength $\phi$ Factor	.....	0.75
	<b>- Side</b>	<b>+ Side</b>
One-way Shear $V_{ux}$	... 309.4	31.3 kip
Shear Strength $\phi V_{cx}$	.. 283.9	283.9 kip
Max. One-way Shear Ratio $V_u/\phi V_c$	..	1.09 <b>NG</b>

- Punching Shear (Comb: 1.2D+1.6L+0.5S)

Unbalanced Moment Factor $\gamma_{vx}$	... 0.40
Punching Shear due to Axial	.... 65.9 psi
Punching Shear due to $M_z$	..... 0.0 psi
Punching Shear Stress $V_u$	..... 65.9 psi
Effective Perimeter $b_o$	..... 240.0 in
Average Effective Depth $d$	..... 36.0 in
Punching Shear Strength $\phi V_c$	.. 164.3 psi
Punching Shear Ratio $V_u/\phi V_c$	..... 0.40 <b>OK</b>

- Transv. Flexure (Comb: 1.2D+1.6L+0.5S)

Under-strength $\phi$ Factor	.....	0.90
Footing Effective Length	.....	8.00 ft
<i>Use 6 #6 Bars Parallel to Z (Top) , d = 36.6 in</i>		
<i>Use 9 #8 Bars Parallel to Z (Bot) , d = 35.5 in</i>		
Bottom Steel Min. Area Ratio	.....	0.97 <b>OK</b>

	<b>Top</b>	<b>Bot</b>	
Bending Moment $M_{ux}$	.. 0.0	390.9	k-ft
Bending Strength $\phi M_{nx}$	431.2	1107.9	k-ft
Max. Bending Ratio $M_{ux}/\phi M_{nx}$	.....	0.35	<b>OK</b>
Top Z-Bars Develop. Length Ratio	..	0.00	<b>OK</b>
Bot Z-Bars Develop. Length Ratio	..	0.34	<b>OK</b>

**LONGITUDINAL REINF.**

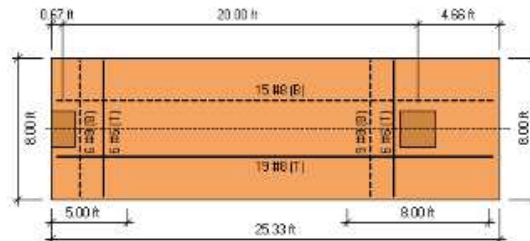
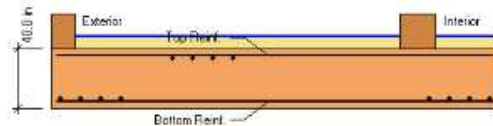
- Long. Flexure (Comb: 1.2D+1.6L+0.5S)

*Use 19 #8 Bars Parallel to X (Top) , d = 37.5 in*  
*Use 15 #8 Bars Parallel to X (Bot) , d = 36.5 in*

	<b>Top</b>	<b>Bot</b>	
Min. Steel Area Ratio	... 0.80	0.48	<b>OK</b>
Bending Moment $M_{uz}$	.. 2105.5	514.9	k-ft
Bending Strength $\phi M_{nz}$	2408.3	1868.7	k-ft
Max. Bending Ratio $M_{uz}/\phi M_{nz}$	.....	0.87	<b>OK</b>
Ext. Bot X-Bars Dev. Length Ratio	..	0.06	<b>OK</b>
Int. Bot X-Bars Dev. Length Ratio	... 0.22		<b>OK</b>

**LOAD TRANSFER (Comb: 1.2D+1.6L+0.5S)**

Bearing Under-strength $\phi$ Factor	.....	0.65	
	<b>Ext.</b>	<b>Int.</b>	
Compressive Stress $P_u$	1.3	1.3	ksi
Column Bearing $\phi P_n$	2.6	2.4	ksi <b>OK</b>
Footing Bearing $\phi P_n$	2.0	3.6	ksi <b>OK</b>
Shear Force $V_u$	<b>0.0</b>	<b>0.0</b>	kip
Shear Friction $\phi V_n$	95.0	95.0	kip <b>OK</b>
Dowel Steel Area $A_s$	<b>3.52</b>	<b>3.52</b>	in <sup>2</sup>
Min. Steel Area $A_s$ min	1.92	2.88	in <sup>2</sup> <b>OK</b>
Dev. Length Ratio at Col.	0.47	0.47	<b>OK</b>
Dev. Length Ratio at Ftg.	0.27	0.27	<b>OK</b>



**UPLIFT CALCS (Comb: 0.6D+0.7E)**

Uplift Force $P$	.....	0.0	kip
Pedestals Selfweight	.....	0.0	kip
Footing Selfweight	.....	60.8	kip
Soil Cover Weight	.....	9.5	kip
Downward Force $W$	.....	370.2	kip
Uplift Safety Factor	.....	99.99	> 1.0 <b>OK</b>