

Spread Footing Verification Example

Reference: Reinforced Concrete – Mechanics and Design, 5th Edition, by Wright and MacGregor, Prentice Hall, 2009. Example 15-2.

A square spread footing supports an 18-in square supporting a service dead load of 400 kips and a service live load of 270 kips. The column is built with 5000-psi concrete and has 8 #9 longitudinal bars with $f_y = 60$ ksi. Design the footing to be constructed using 3000-psi concrete. The top of the footing is covered with 6-in of fill with a density of 120 pcf and a 6-in basement floor with a load of 100 psf. The allowable pressure of the soil is 6000 psf.

$$U = 1.4 D = 1.4 \times 400 = 560 \text{ kips}$$

$$U = 1.2 D + 1.6 L = 1.2 \times 400 + 1.6 \times 270 = 912 \text{ kips (controls)}$$

- Try an 11'-2" x 32" thick footing ($d = 28"$). Check punching shear.

$$\text{Factored net soil pressure} = 912/11.17^2 = 7.31 \text{ ksf}$$

The critical shear perimeter is a square which side is $18" + 28" = 46"$

$$V_u = 7.31[11.17^2 - (46/12)^2] = 805 \text{ kips}$$

$$\phi V_c = 0.75 \times 4 \sqrt{3000} \times 46 \times 4 \times 28 = 847 \text{ kips} > V_u \text{ OK}$$

- Check one-way shear.

$$V_u = 7.31[11.17 \times (30/12)] = 204 \text{ kips}$$

$$\phi V_c = 0.75 \times 2 \sqrt{3000} \times 134 \times 28 = 308 \text{ kips} > V_u \text{ OK}$$

- Design the flexural reinforcement.

$$M_u = 7.31[11.17 \times (58/12)^2 / 2] = 954 \text{ kips}$$

Try 11 #8 bars each way ($A_s = 8.69 \text{ in}^2$)

$$a = 8.69 \times 60 / (0.85 \times 3 \times 134) = 1.53 \text{ in (tension controlled)}$$

$$\phi M_n = 0.9 \times 8.69 \times 60 (28 - 1.53/2) = 1065 \text{ k-ft} > M_u \text{ OK}$$

- Check the development.

The clear spacing exceeds $2d_b$ and the clear cover exceeds d_b , therefore

$$L_d = 60000 / (20 \sqrt{3000}) d_b = 54.8 \times 1" = 54.8" \text{ OK}$$

- Design the column-footing joint.

The allowable bearing on the footing is $0.85 \times 0.65 \times 3 \times 18^2 \times 2 = 1070$ kips

The allowable bearing on the base of the column is $0.85 \times 0.65 \times 5 \times 18^2 = 895$ kips (controls)

$$\text{Area of dowels required} = (912 - 895) / (0.65 \times 60) = 0.44 \text{ in}^2$$

$$\text{Area of dowels minimum} = 0.005 \times 18^2 = 1.62 \text{ in}^2 \text{ (controls)}$$

Use 4 #6 dowels. Extend dowels 25" into column.

GEOMETRY

Footing Length (X-dir)	11.17	ft	
Footing Width (Z-dir)	11.17	ft	
Footing Thickness	32.0	in	OK
Soil Cover	0.50	ft	
Column Length (X-dir)	18.0	in	
Column Width (Z-dir)	18.0	in	
Offset (X-dir)	0.0	in	OK
Offset (Z-dir)	0.0	in	OK
Pedestal Height	N. A.	ft	

SOIL PRESSURES (Comb: D+L)

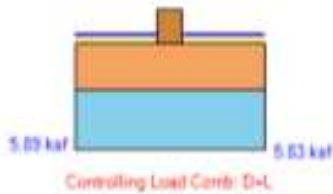
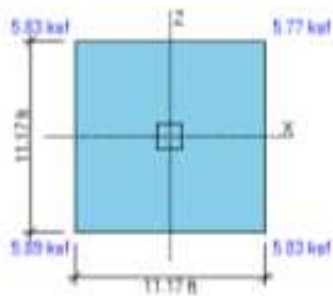
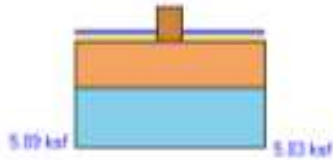
Gross Allow. Soil Pressure ..	6.00	ksf
Soil Pressure at Corner 1	5.89	ksf
Soil Pressure at Corner 2	5.83	ksf
Soil Pressure at Corner 3	5.77	ksf
Soil Pressure at Corner 4	5.83	ksf
Bearing Pressure Ratio	0.98	OK
Ftg. Area in Contact with Soil ...	100.0	%
X-eccentricity / Ftg. Length	0.00	OK
Z-eccentricity / Ftg. Width	0.00	OK

APPLIED LOADS

	Dead	Live	RLive	Snow	Wind	Seismic	
Axial Force P	400.0	270.0	0.0	0.0	0.0	0.0	kip
Moment about X Mx ..	0.0	0.0	0.0	0.0	0.0	0.0	k-ft
Moment about Z Mz ..	0.0	0.0	0.0	0.0	0.0	0.0	k-ft
Shear Force Vx	0.0	0.0	0.0	0.0	0.0	0.0	kip
Shear Force Vz	0.0	0.0	0.0	0.0	0.0	0.0	kip

OVERTURNING CALCULATIONS (Comb: 0.6D+1W)

OVERTURNING				RESISTING				
	Force	Arm	Moment		Force	Arm	Moment	
	kip	ft	k-ft		kip	ft	k-ft	
- About X-X				- About X-X				
Moment Mx	---	---	0.0	Footing Weight ..	29.9	5.59	167.2	
Shear Force Vz	0.0	2.67	0.0	Column Weight ..	0.0	5.59	0.0	
Rh = 0.0		OTM = 0.0		Soil Cover	4.4	5.59	24.6	
- About Z-Z				- About Z-Z				
Moment Mz	---	---	0.0	Axial Force P	240.0	5.59	1340.4	
Shear Force Vx	0.0	2.67	0.0	Rv = 274.4		RM = 1532.3		
Rh = 0.0		OTM = 0.0		- About Z-Z				
		X-X	Z-Z	Footing Weight ..	29.9	5.59	167.2	
Arm of Vertical Resultant =		5.59	5.59	Column Weight ..	0.0	5.59	0.0	
Overturning Safety Factor =	99.99	99.99	> 1.5	OK	Soil Cover	4.4	5.59	24.6
				Axial Force P	240.0	5.59	1340.4	
				Rv = 274.4		RM = 1532.3		



SLIDING (Comb. 0.6D+1W)

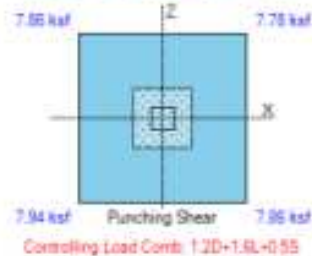
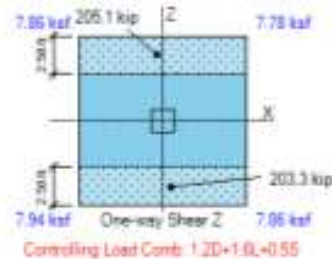
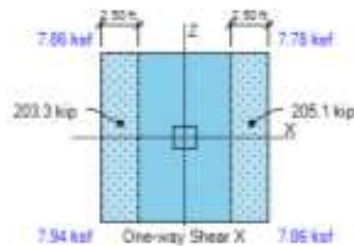
Footing-Soil Friction Coeff.	0.45
Friction Force at Base	123.5 kip
Passive Pressure Coeff. Kp	2.77
	<u>X-X</u> <u>Z-Z</u>
Passive Force @ Ftg ...	18.2 18.2 kip
Horiz. Resisting Force	141.6 141.6 kip
Horiz. Sliding Force	0.0 0.0 kip
Sliding Safety Factor ...	99.99 99.99 > 1.5 OK

UPLIFT CALCS (Comb: 0.6D+0.7E)

Uplift Force P	0.0 kip
Pedestal Selfweight	0.0 kip
Footing Selfweight	29.9 kip
Soil Cover Weight	4.4 kip
Downward Force W	34.4 kip
Uplift Safety Factor	99.99 > 1.0 OK

PUNCHING SHEAR (Comb: 1.2D+1.6L+0.5S)

Unbalanced Moment Factor γ_{vx} ...	0.40
Unbalanced Moment Factor γ_{vz} ...	0.40
Punching Shear due to Axial	178.4 psi
Punching Shear due to M_x	0.0 psi
Punching Shear due to M_z	0.0 psi
Punching Shear Stress V_u	178.4 psi
Effective Perimeter b_o	184.0 in
Average Effective Depth d	28.0 in
Column Location Factor α_s	40 (Interior)
Column Aspect Ratio β	1.00
Punching Shear Strength ϕV_c ..	332.2 psi
Punching Shear Ratio $V_u/\phi V_c$	0.54 OK



ONE-WAY SHEAR (Comb: 1.2D+1.6L+0.5S)

	- Side	+ Side	
One-way Shear V_{ux} ...	203.3	205.1	kip
One-way Shear V_{uz} ...	203.3	205.1	kip
Under-strength ϕ Factor	0.75		
One-way Shear Strength ϕV_{cx}	302.8		kip OK
One-way Shear Strength ϕV_{cz}	313.9		kip OK
Max. One-way Shear Ratio $V_u/\phi V_c$..	0.68		OK

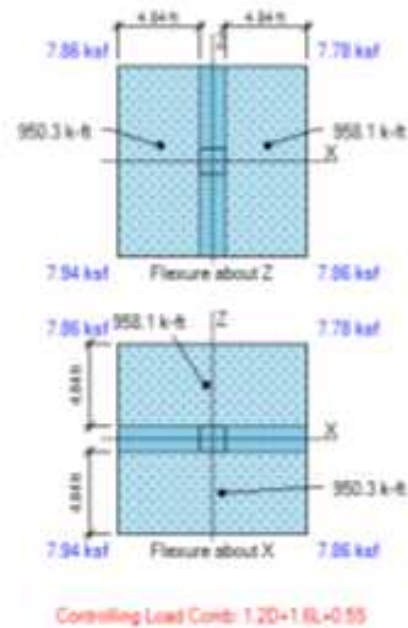
FLEXURE (Comb: 1.2D+1.6L+0.5S)

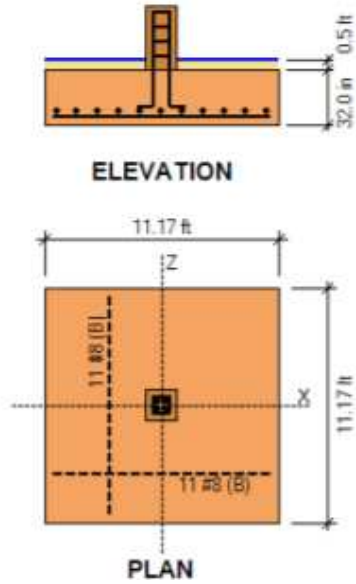
- Top Bars -		- Side	+ Side	
Bending Moment - M_{ux} ...	0.0	0.0		k-ft
Bending Moment - M_{uz} ...	0.0	0.0		k-ft
<i>No Top Reinforcement Provided at the Footing</i>				
<i>Use Plain Concrete Flexural Strength at Top</i>				
X-Bars Development Length Ratio ..	N.A.			
Z-Bars Development Length Ratio ..	N.A.			
Min. Top Steel Area Ratio	N.A.			
Under-strength ϕ Factor	0.55			
Bending Strength - ϕM_{nx}	287.1			k-ft OK
Bending Strength - ϕM_{nz}	287.1			k-ft OK
Max. Bending Ratio - $M_u/\phi M_n$	0.00			OK

- Bottom Bars -		- Side	+ Side	
Bending Moment + M_{ux} ...	950.3	958.1		k-ft
Bending Moment + M_{uz} ...	950.3	958.1		k-ft
<i>Use 11 #8 Bars Parallel to X (Bot) , d = 27.5 in</i>				
<i>Use 11 #8 Bars Parallel to Z (Bot) , d = 28.5 in</i>				
X-Bars Development Length Ratio ..	0.59			OK
Z-Bars Development Length Ratio ..	0.59			OK
Min. Bottom Steel Area Ratio	0.89			OK
Under-strength ϕ Factor	0.90			
Bending Strength + ϕM_{nx}	1084.6			k-ft OK
Bending Strength + ϕM_{nz}	1045.5			k-ft OK
Max. Bending Ratio + $M_u/\phi M_n$	0.92			OK

TRANSFER (Comb: 1.2D+1.6L+0.5S)

Bearing Under-strength ϕ Factor	0.65
<i>Use 4 #6 x 2.00 ft hooked dowels , $A_s = 1.76$ in²</i>	
Compressive Stress P_u	2.8 ksi
Column Bearing Strength ϕP_n ...	3.0 ksi OK
Footing Bearing Strength ϕP_n ...	3.5 ksi OK
Shear Force Transfer V_u	0.0 kip
Shear Friction Strength ϕV_n	47.5 kip OK
Min. Steel Area $A_s = 0.005 A_1$...	1.62 in ² OK
Develop. Length Ratio at Column	0.64 OK
Develop. Length Ratio at Footing	0.31 OK





DESIGN CODES

Concrete Design	ACI 318-08
Load Combinations	ASCE 7-05

MATERIALS

Column Concrete f_c	5.0	ksi
Column Dowels f_y	60.0	ksi
Column Ties f_y	60.0	ksi
Footing Concrete f_c	3.0	ksi
Footing Rebars f_y	60.0	ksi
Soil Cover Density	120.0	pcf